

Low Power Circuit Techniques for Energy Harvesting Applications

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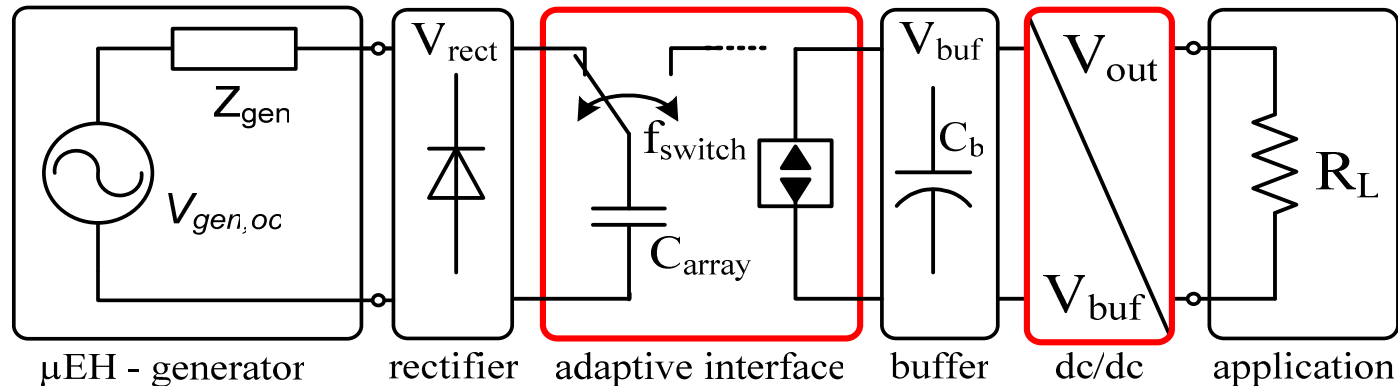


- Motivation: Two-Stage Power Processing
- Interface for Inductive Transducers
 - Operation Principle
 - Measurement Results
- Interface for Piezoelectric Transducers
 - Operation Principle
 - Measurement Results
- Low-Voltage Circuits and Converters
 - 0.5 V Amplifier
 - Comparator-less PWM
- Conclusion

- Motivation & Application Examples
- Rectification
 - Passive rectification
 - Active diodes
 - Floating gate enhanced CMOS-switches
- Interface for Electromagnetic Transducers
 - Load matching approach
 - Switched-capacitor converter
- Low-Voltage Circuits and Converters
 - 0.5 V amplifier
 - Comparator-less PWM

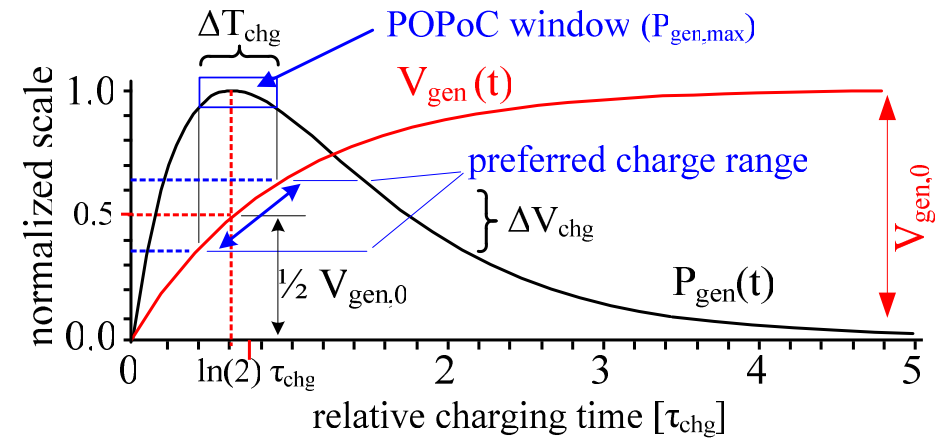
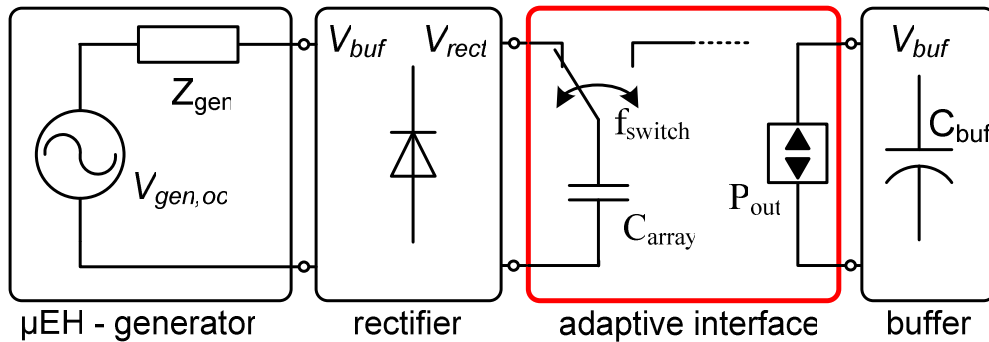
Two-Stage Power Processing

- Vibration energy harvesting (inductive – piezoelectric)
- 1st stage: generator interface for efficient harvesting



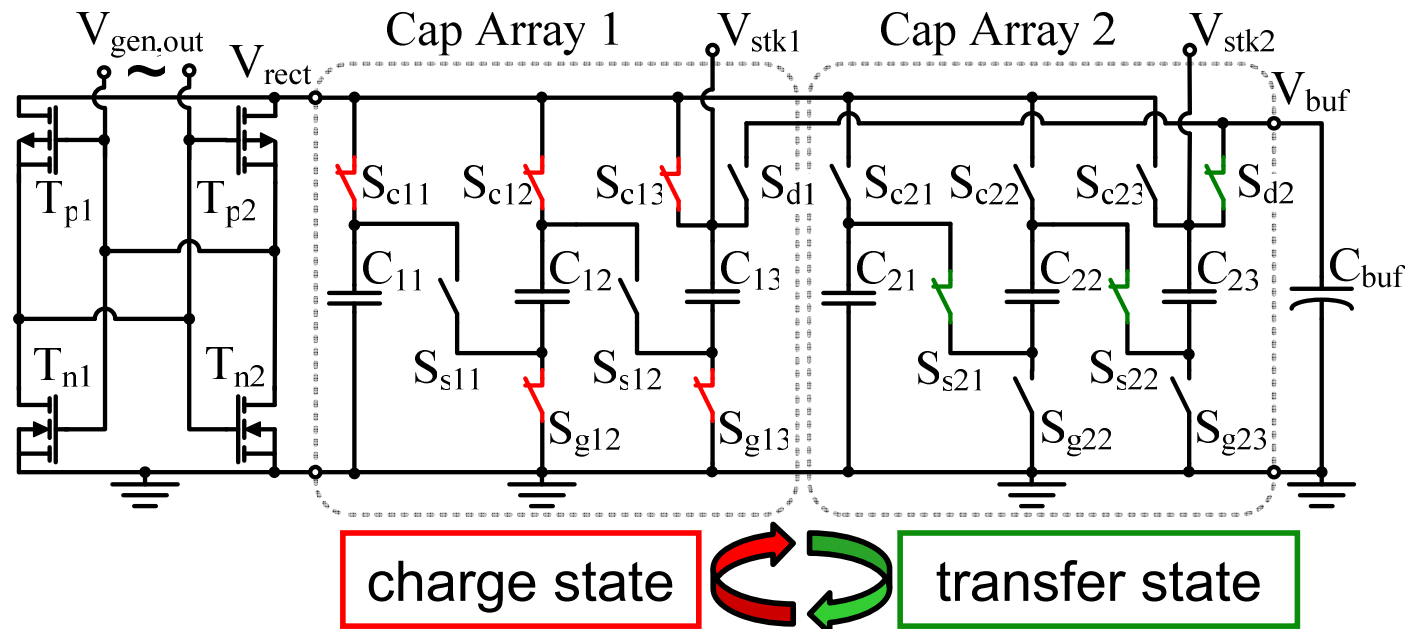
- Load matching detection
- Fluctuant buffer voltage
- 2nd stage: DC/DC voltage conversion
 - PWM control by modulated digital gate delays
 - Dedicated building blocks for low-voltage operation
 - Stable and controlled output voltage

Adaptive Switched Capacitor Interface for Inductive Generators

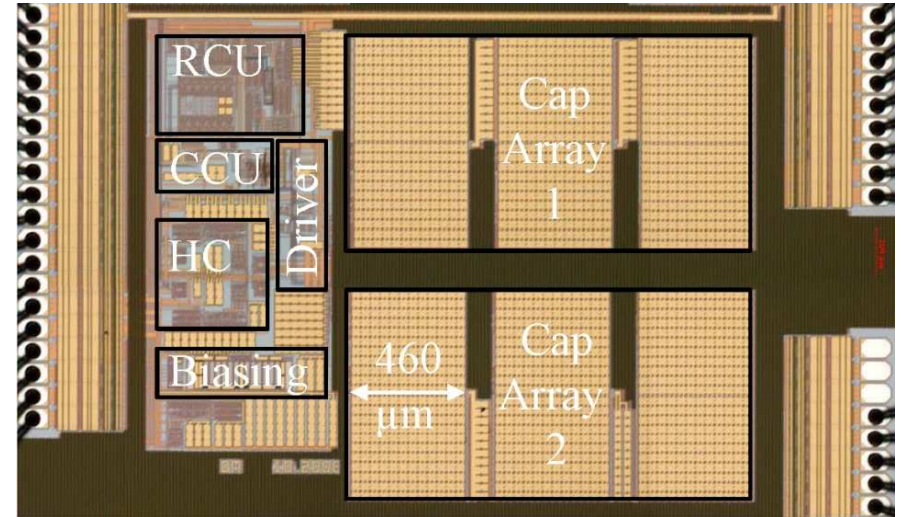
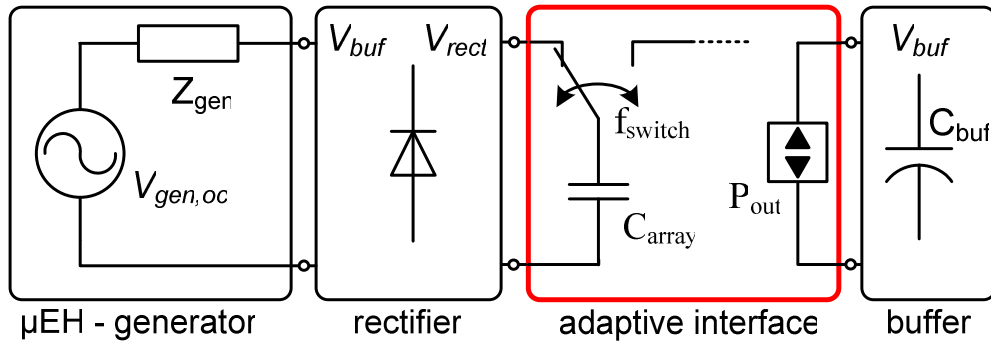


Requirement 1:
Load/ impedance
matching

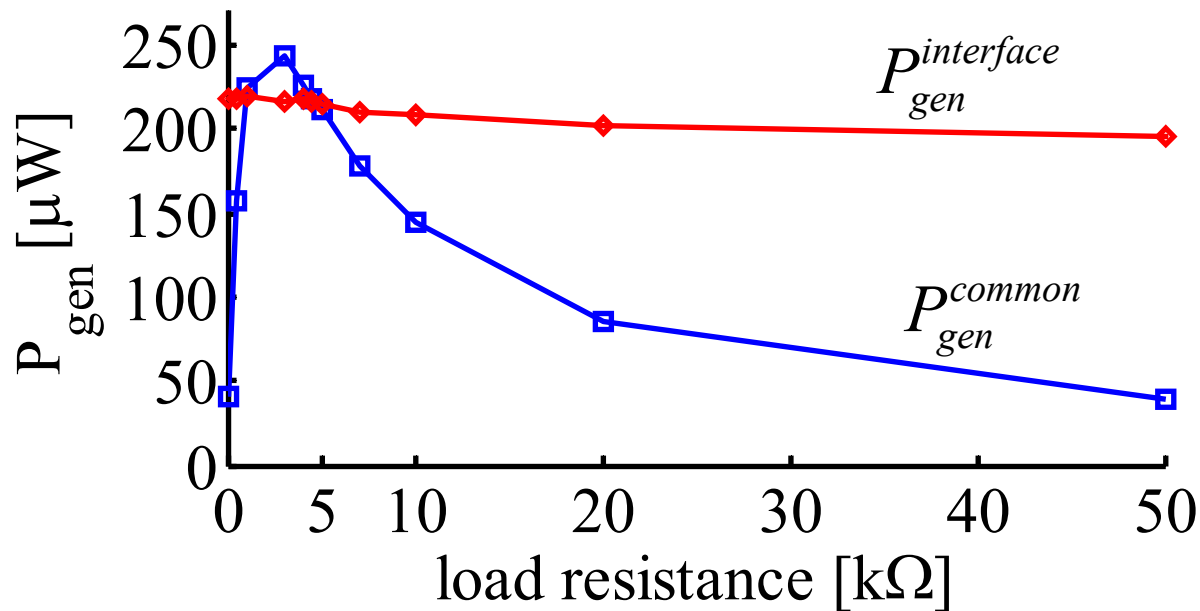
Requirement 2:
Independence of
buffer voltage



Adaptive Switched Capacitor Interface



[D. Maurath, ESSCIRC 2009]



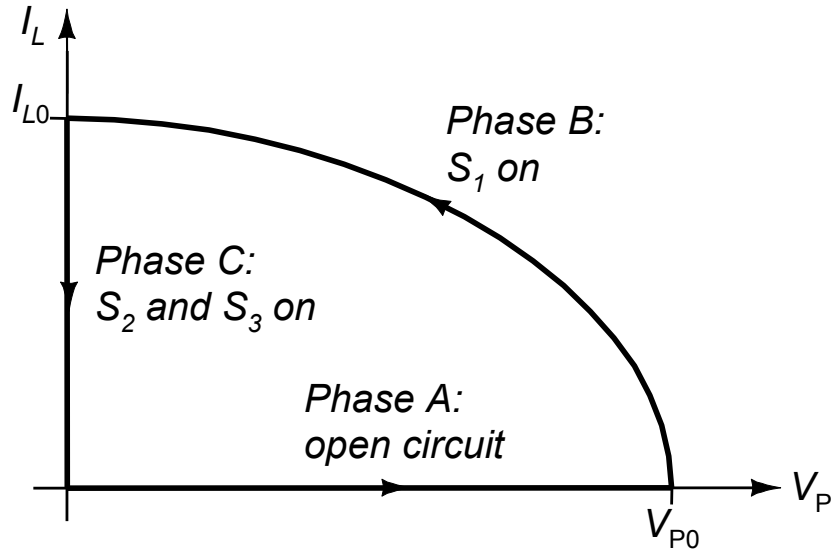
Generator parameters:

R_{gen}	2,05 kΩ
f_{res}	168 Hz
$V_{gen,0}^{peak}$	2.0 V
P_{max}	250 μW

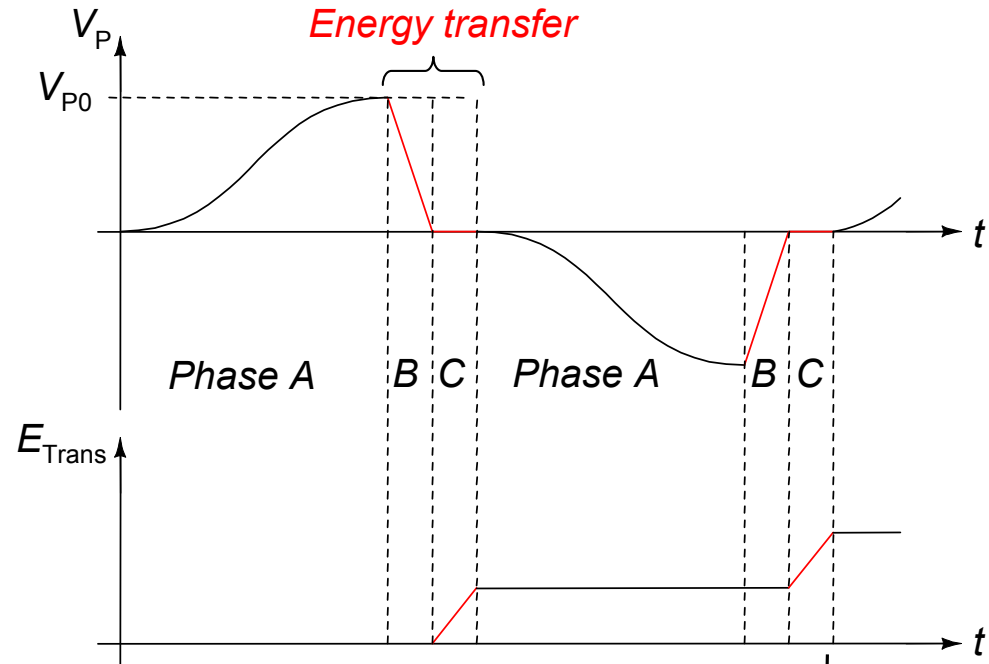
Interface for Piezoelectric Generators



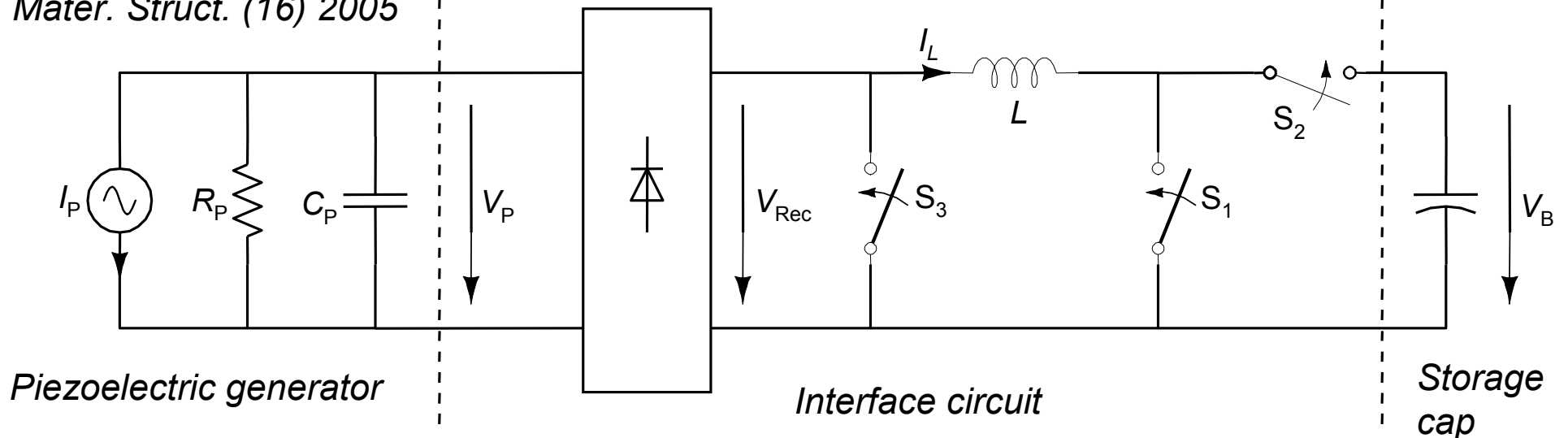
State diagram



Time diagram

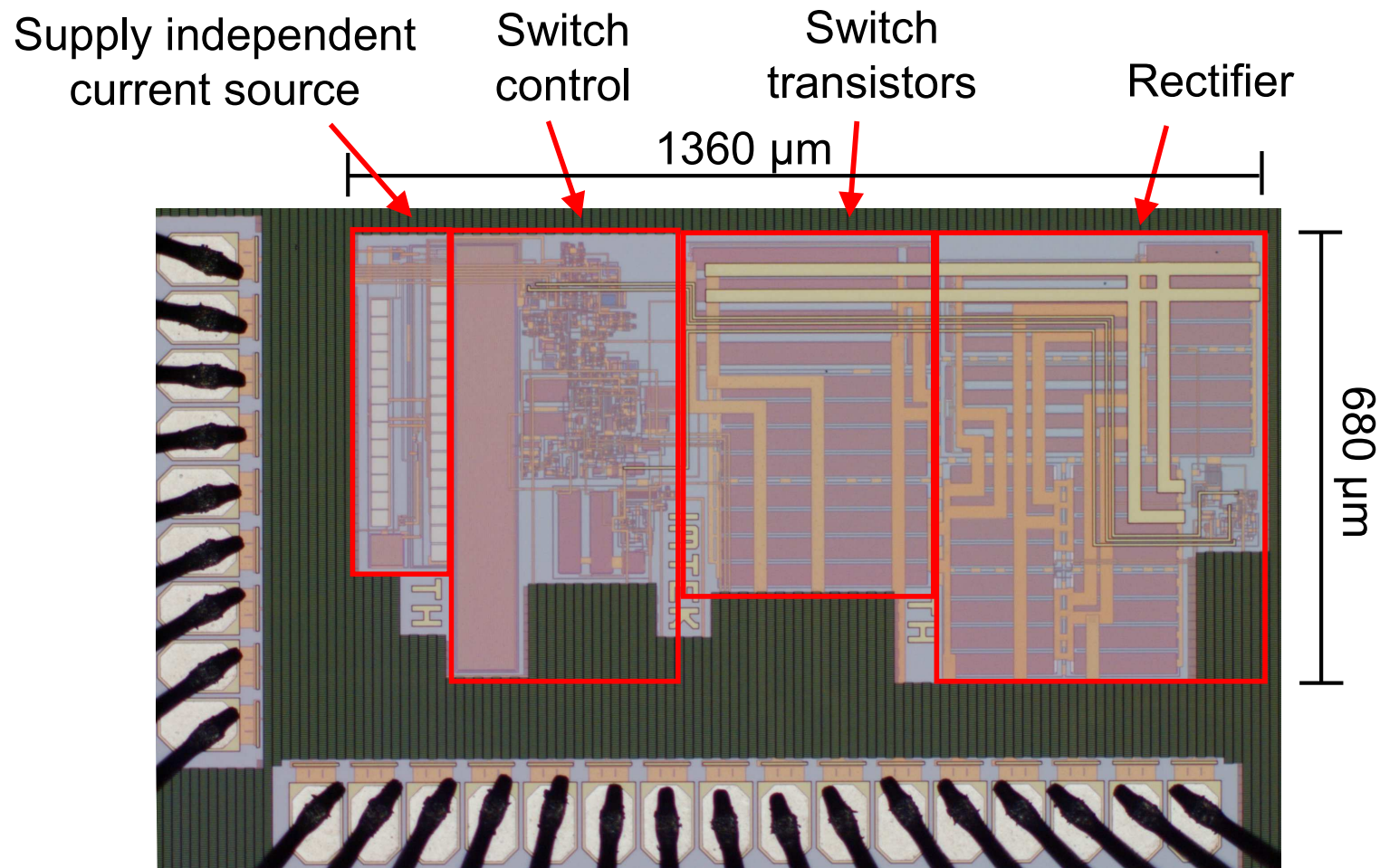


“Synchronous electric charge extraction”, Lefeuvre et al., *J. Int. Mater. Struct.* (16) 2005

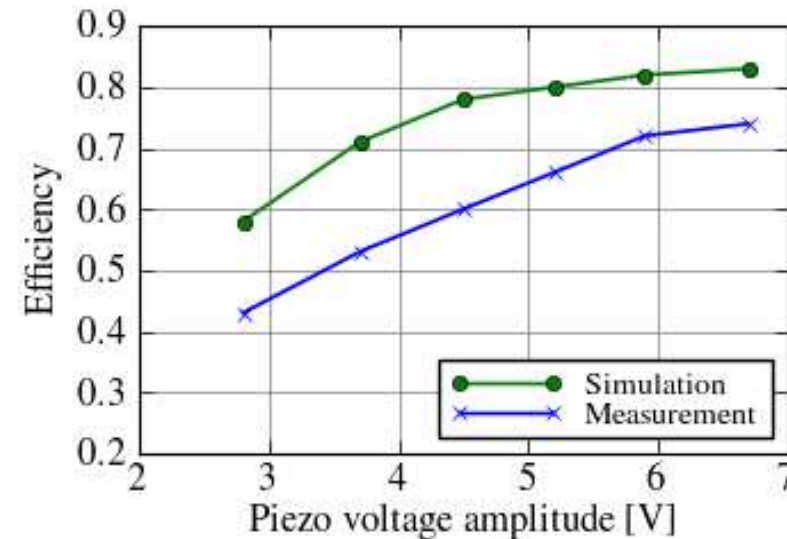
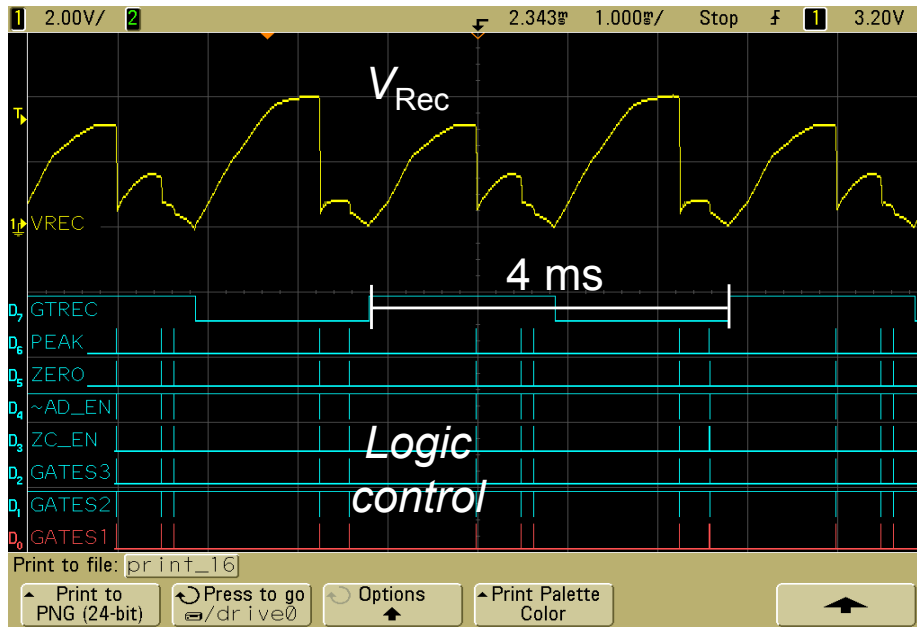


Chip Microphotograph

- Process: 0.35 μm with high voltage option
- Active area: 0.92 mm^2



Simulation vs. Measurement Results

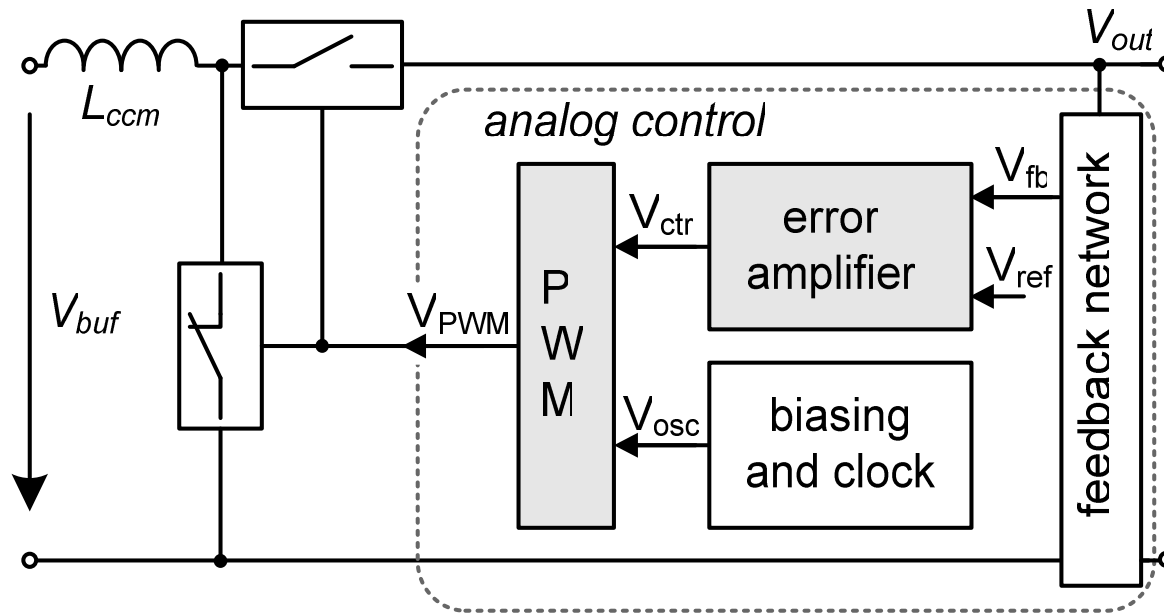


Parameters:

$L=1\text{mH}$, $V_B=2\text{V}$, $C_P=12\text{nF}$,
 $R_P=800\text{k}\Omega$, $f_P=250\text{Hz}$

- Proper peak detection for varying V_P
- Measured efficiency lower than simulated due to nonlinear parasitic losses which are not modelled

Chip specifications		
	Simulation	Measurement
Battery voltage V_B	1.3V ... 3.5V	1.3V ... 2V
Average power consumption	2.5 μ W	tbd
Piezo voltage amplitude V_P	1.4V ... 7V	1.5V ... 7V
Piezo frequency f_P	50Hz ... 1000Hz (ca.)	tbd



- Basic building blocks
 - Error amplifier
 - Pulse-width modulator
 - Voltage reference
 - Power-switch driver
- Operation conditions

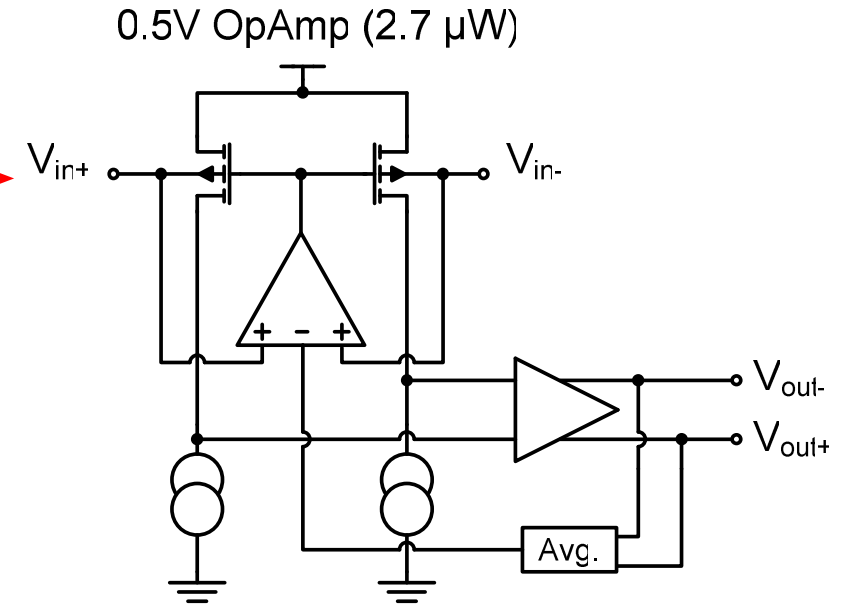
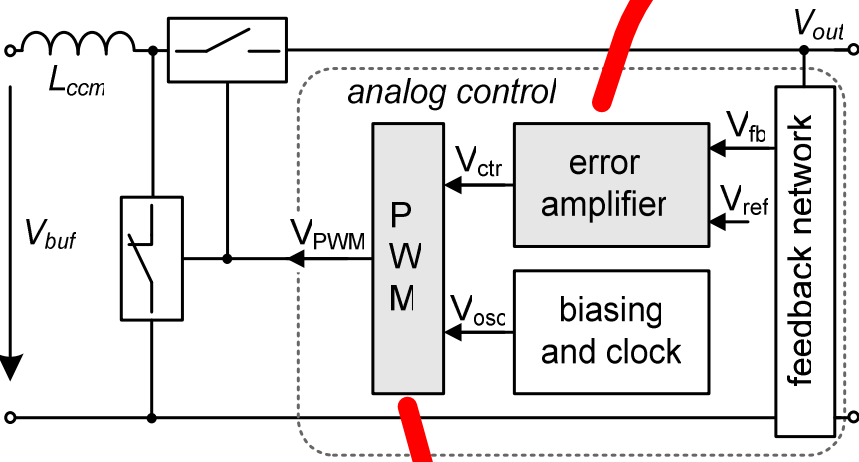
V_{DD} range	0.5 – 3.3 V
Power Loss	some 10 μ W
Load Current	50 μ A – 50 mA
Conv. range	0.5 \rightarrow 3.3 V

- Designing energy-efficient low-voltage circuits
 - Sub-threshold operation
 - Bulk-driven and common-gate amplifiers
 - Creation of an *ultra-low voltage analog library* (IMTEK A_Cells)

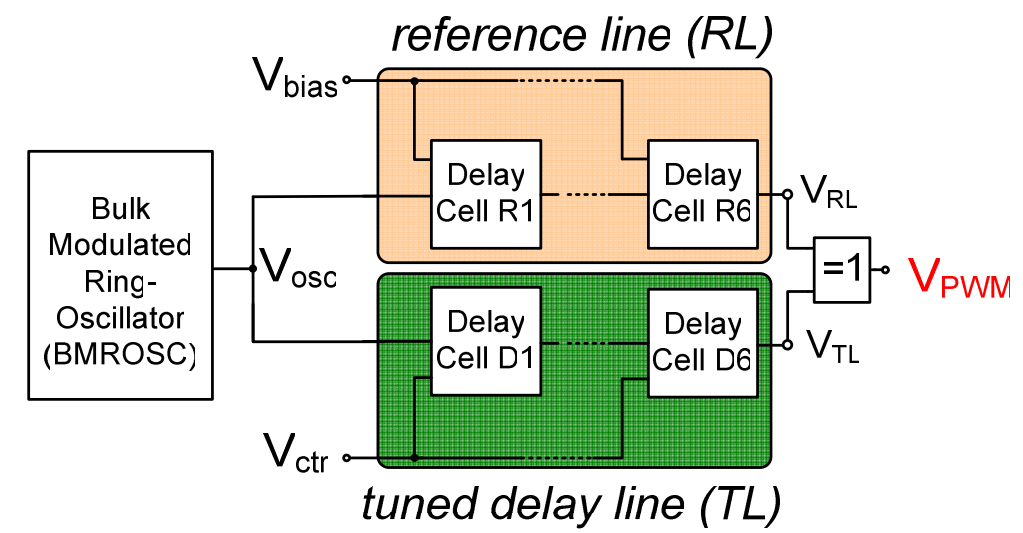
DC/DC Converter - Basic Building Blocks



- Bulk-driven input stage
- No tail: 2-stacked transistors only
- Biasing and feedback



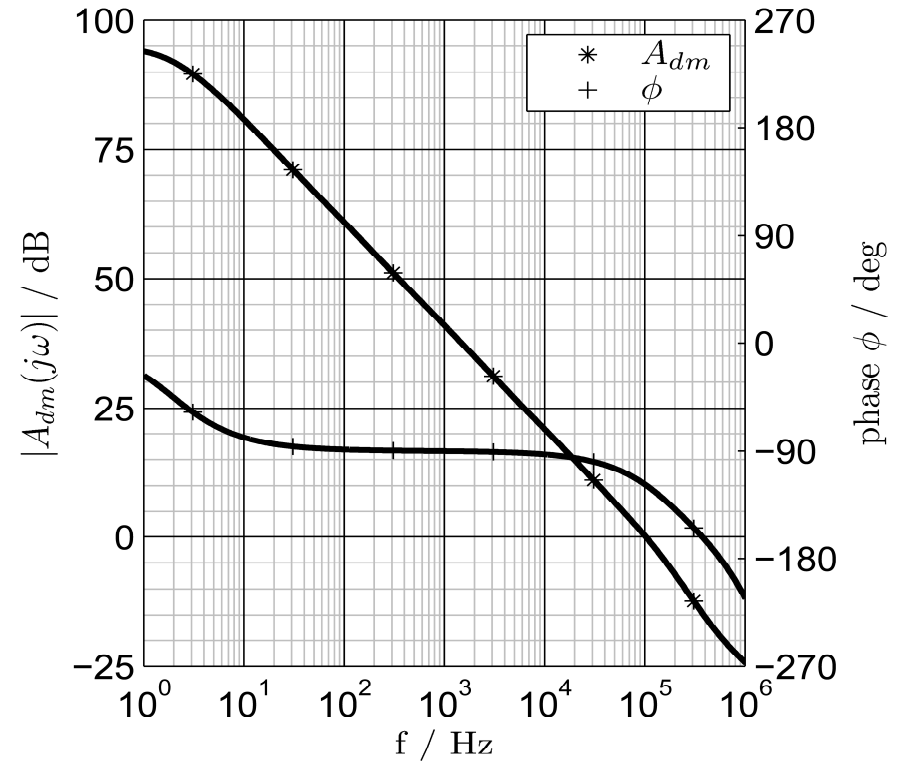
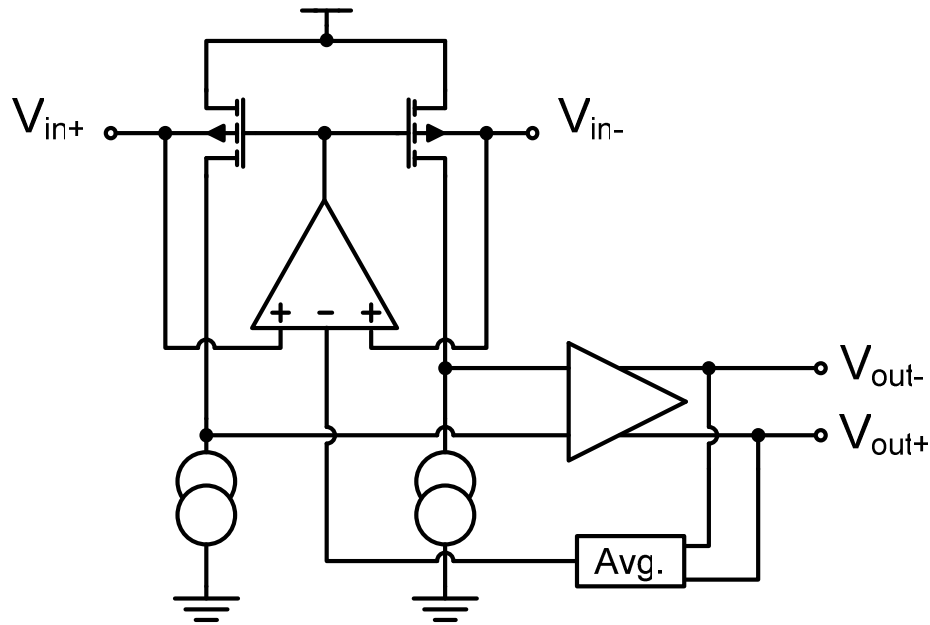
- Comparator-less PWM
- Tuned delay line modulation
- Bulk-driven inverters



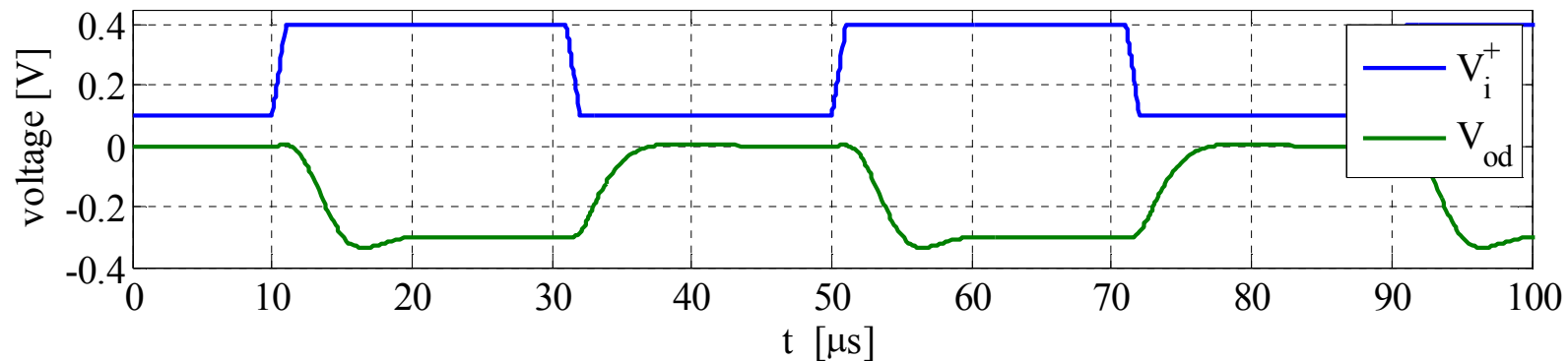
Low-Voltage OpAmp



0.5V OpAmp (2.7 μ W)



25 kHz pulses at non-inverting input v_i^+



Performance Review



Parameter ($V_{DD} = 0.5 \text{ V}$)	Fully Differential ⁴	Single Ended ⁴	Kinget ^{1,5}
DC Gain	93 dB	90 dB	48 dB
GBW, $C_L = 10 \text{ pF}$	100 kHz	100 kHz	2.4 MHz ²
PM, $C_L = 10 \text{ pF}$	60°	60°	45° ²
CMRR @ DC	50 dB	50 dB	-
PSRR @ DC	50 dB	50 dB	-
Inp. ref. noise (@100 Hz)	500 nV/ $\sqrt{\text{Hz}}$	600 nV/ $\sqrt{\text{Hz}}$	220 nV/ $\sqrt{\text{Hz}}$ ³
Power P	2.7 μW	1.7 μW	100 μW
GBW· C_L /P for PM = 45°	0.48	0.97	0.48

¹Shouri Chatterjee, Yannis Tsvividis, and Peter Kinget. 0.5-V analog circuit techniques and their application in OTA and Filter design. *IEEE JOURNAL OF SOLID-STATE CIRCUITS*, 40(12), 2005.

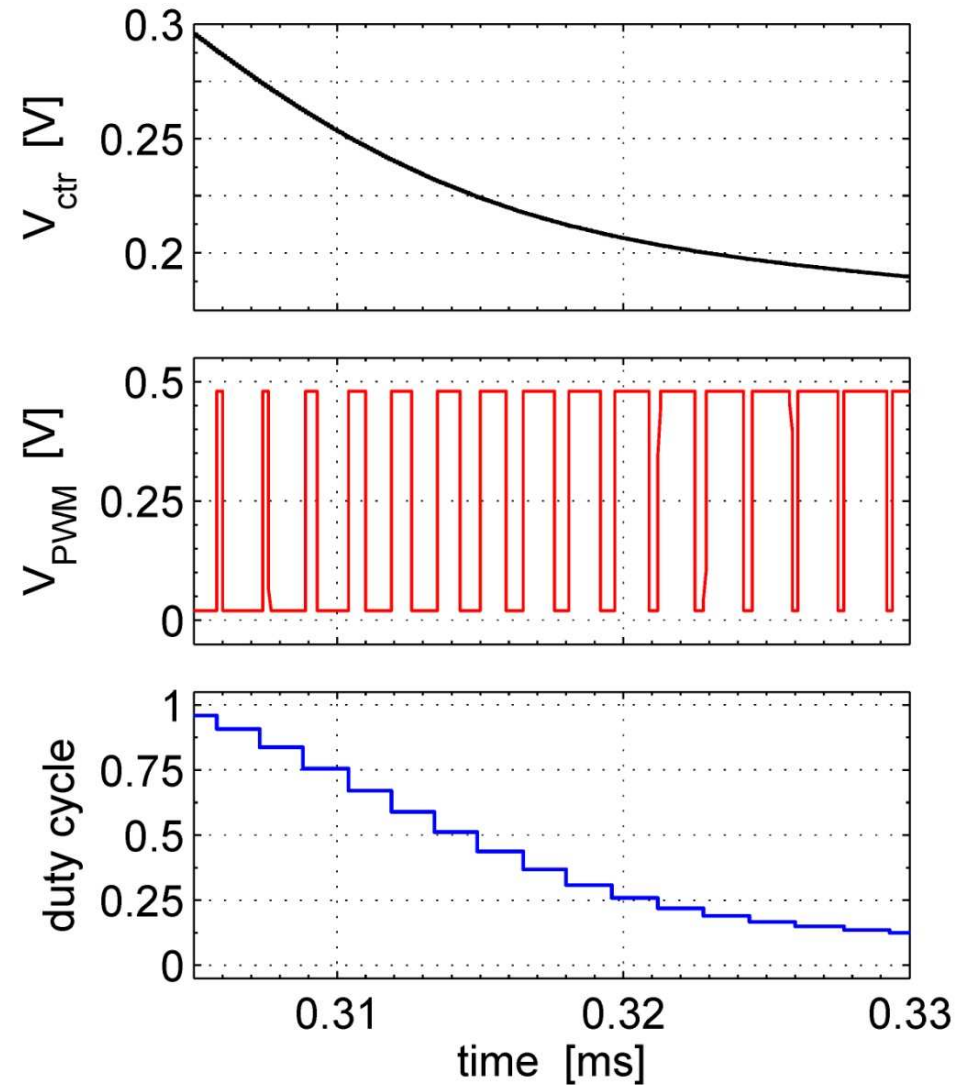
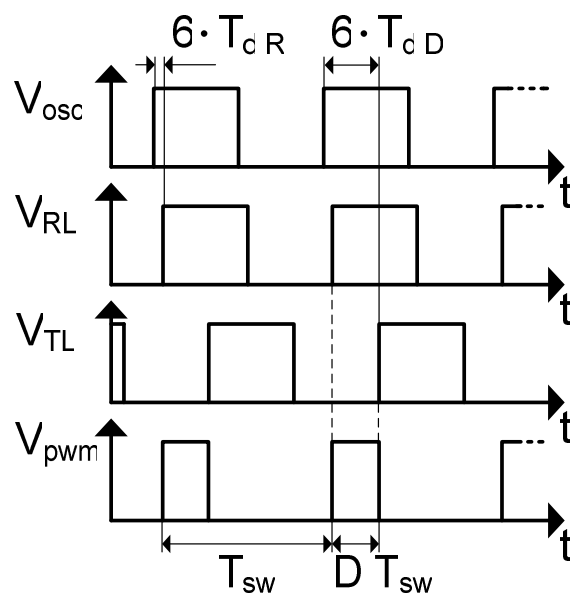
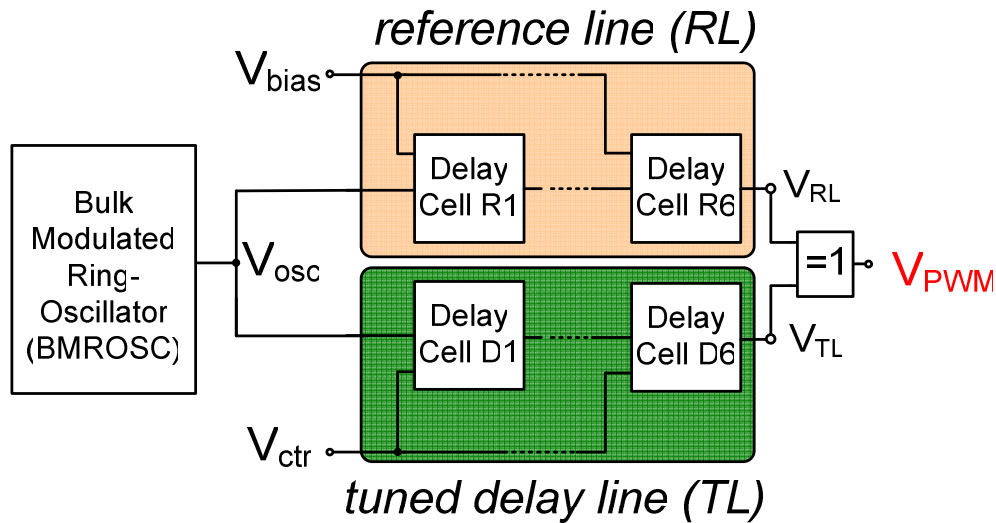
² $C_L = 20 \text{ pF}$

³@ 10 kHz

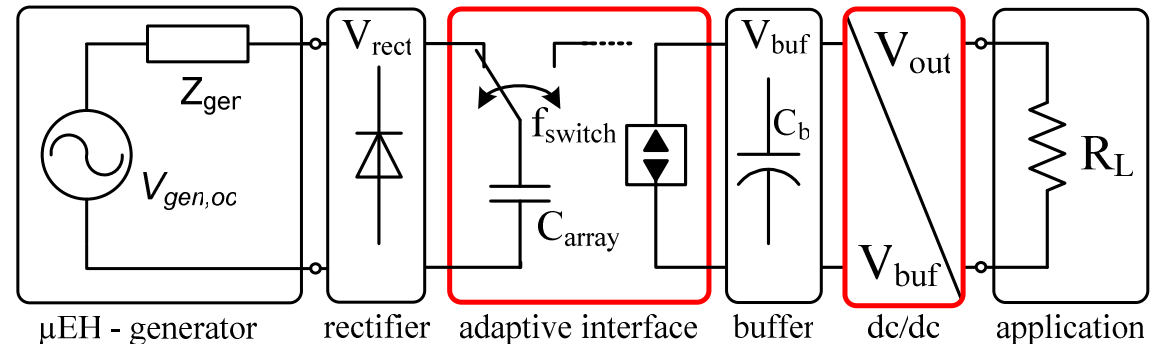
⁴0.35 μm process

⁵0.18 μm process

Delay Line - Pulse Width Modulation



- Low-Voltage Rectification w/o single poly FG transistors
- Adaptive Interface on Chip
 - Measured enhanced impedance matching with charge control
 - Measured decoupling of buffer voltage and generator voltage



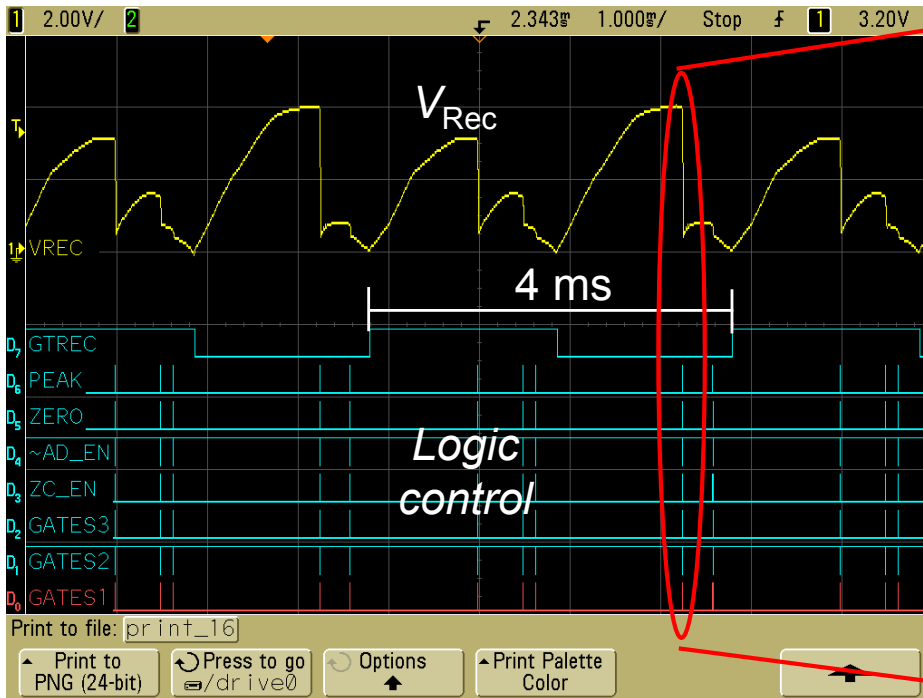
- Building Blocks for DC/DC conversion
 - Delay-based PWM modulation
 - Load adaptive power switch segmentation
- Reduced Supply requirements
 - Less Supply Voltage – high supply voltage flexibility (0.5 – 3.3 V)
 - Low-power consumption

- Two-stage power processing
 - Rectification and adaptive interface for efficient harvesting
 - Ultra-low-power DC/DC converter for stable output voltage
- Adaptive interfaces for inductive and piezoelectric generators
 - Decoupling of buffer and generator
 - Load impedance matching
- Building Blocks for DC/DC conversion
 - 0.5 V amplifier
 - Delay-based PWM modulation
- Reduced Supply requirements
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Thank you for your attention.

Measurement Results

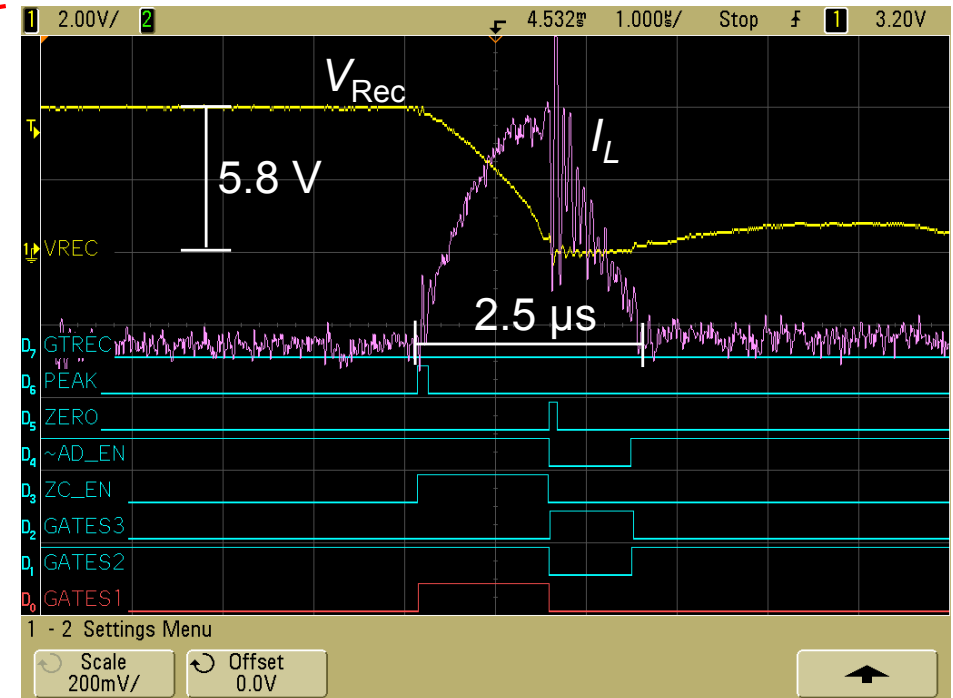
Several periods



Rectifier
Peak
Zero

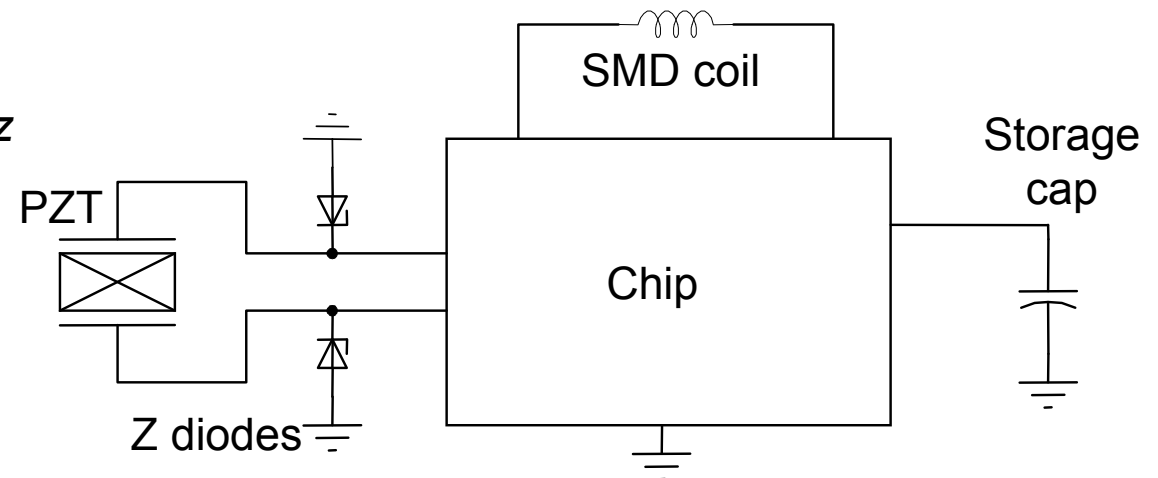
GateS3
GateS2
GateS1

One transfer process



PZT bending generator Q220-A4-103YB (Piezo Systems Inc.), sinusoidal shaker excitation with 40μm amplitude and 250Hz

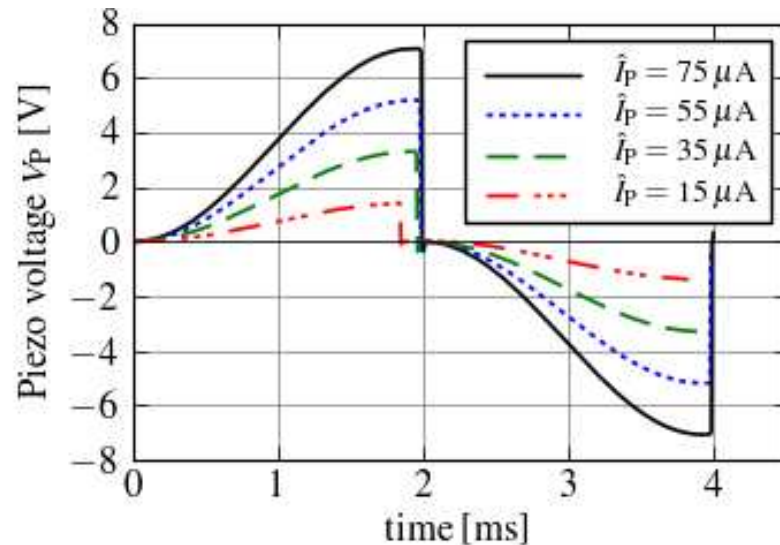
- Proper peak detection
- Proper logic control
- Two peaks per half period due to low R_p



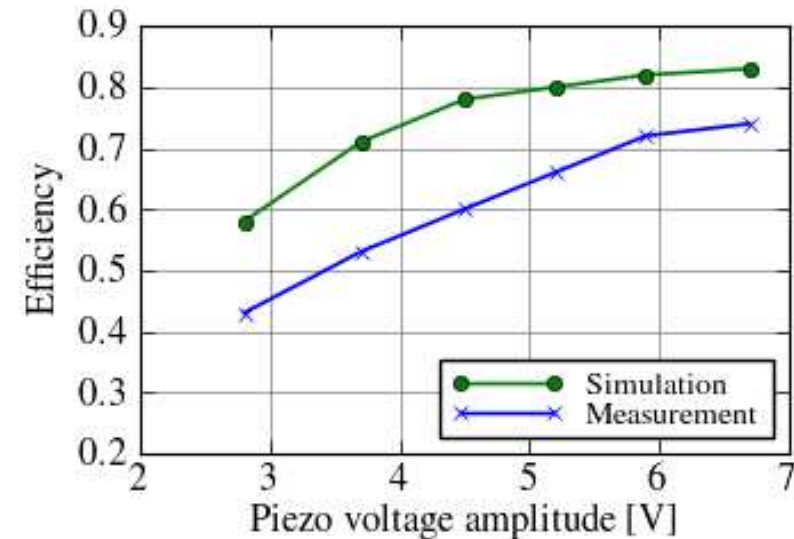
Simulation vs. Measurement Results



Simulation



Simulation & Measurement



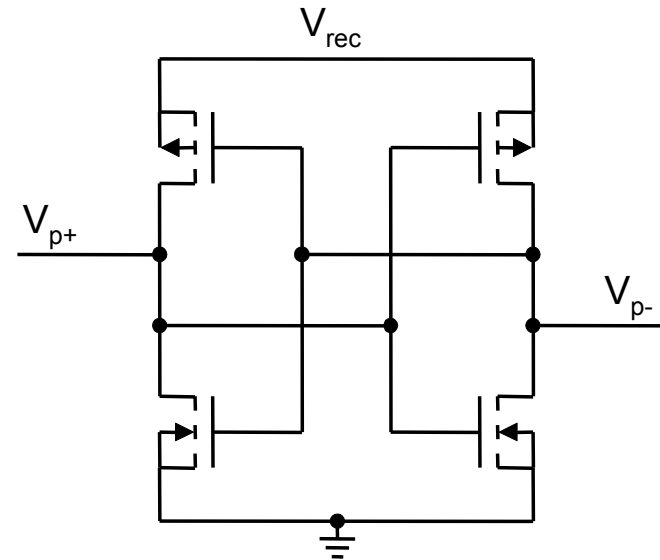
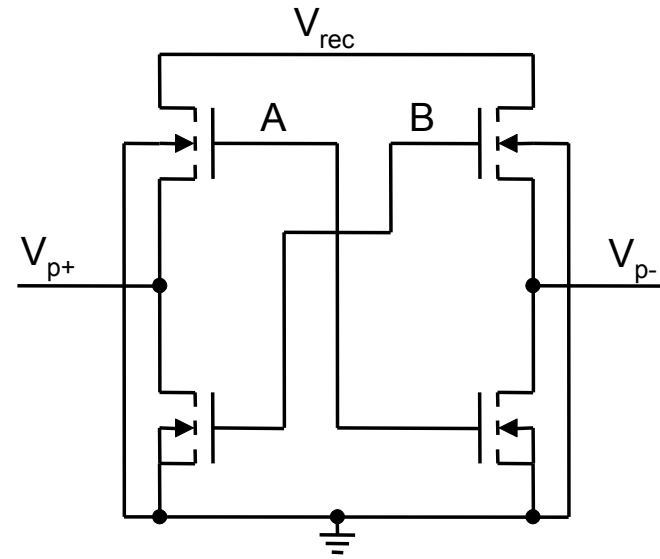
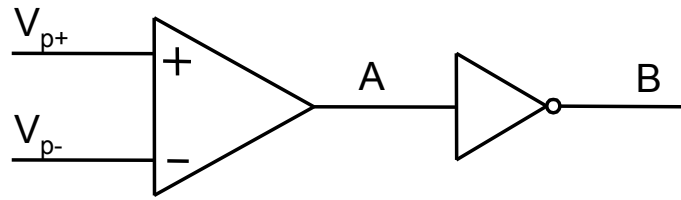
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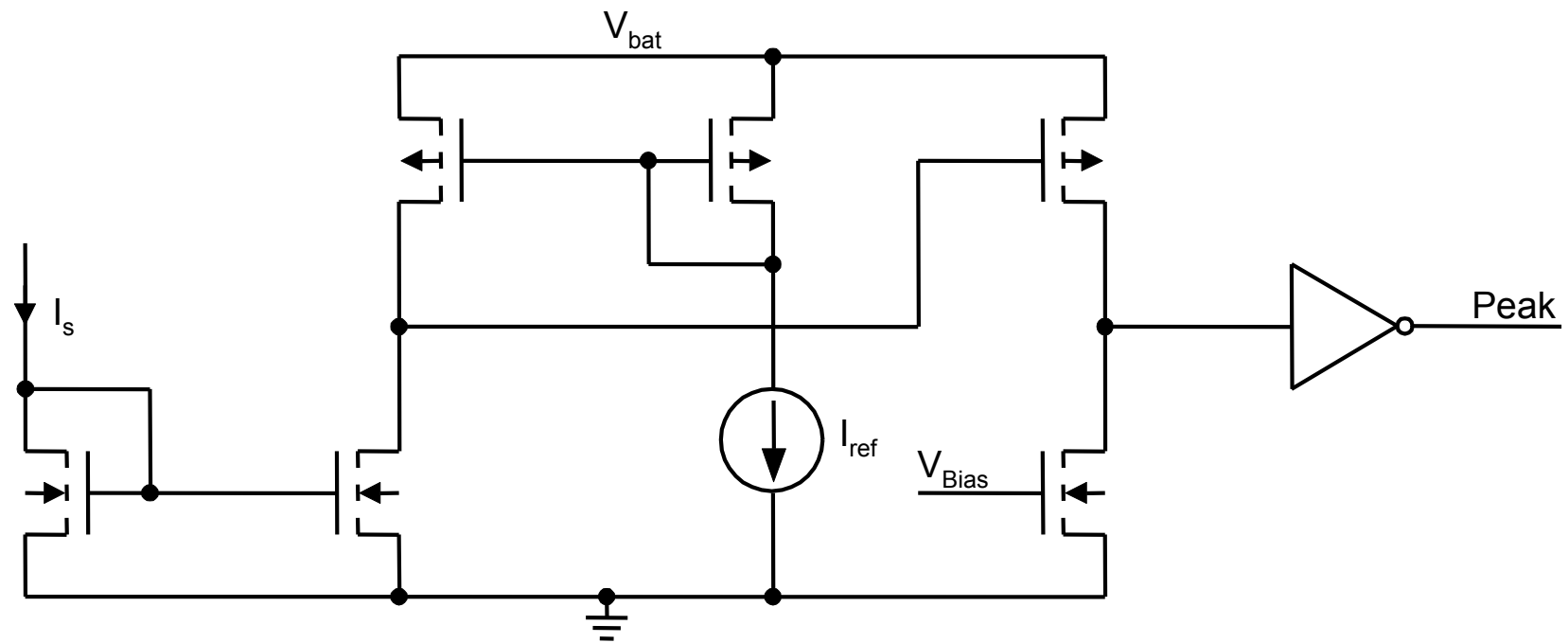
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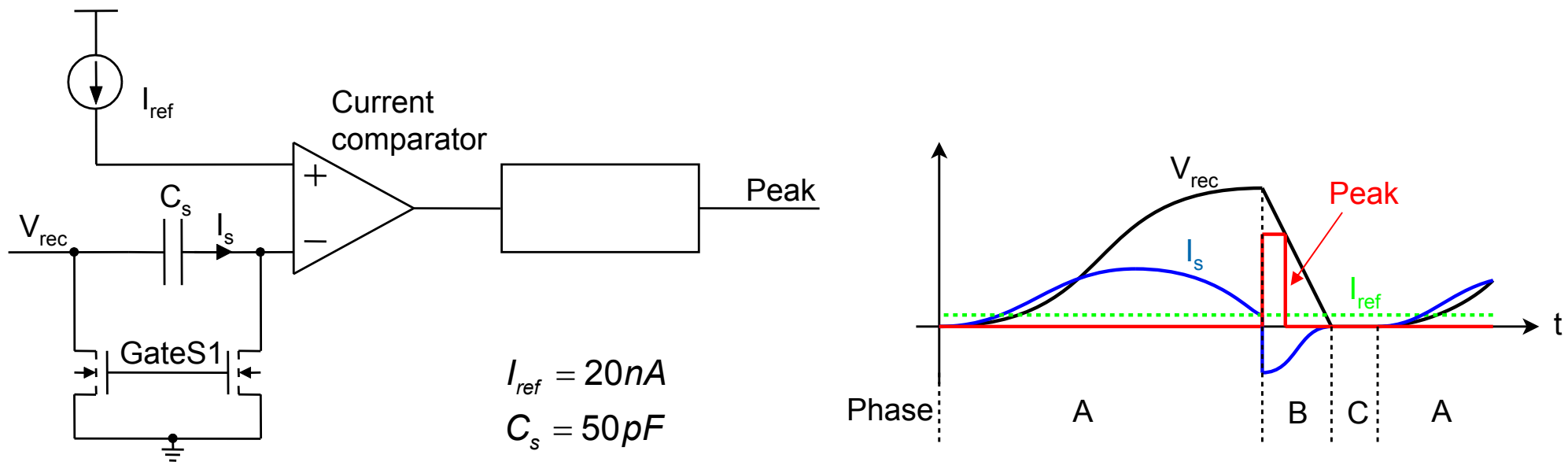
CMOS rectifier



Current comparator

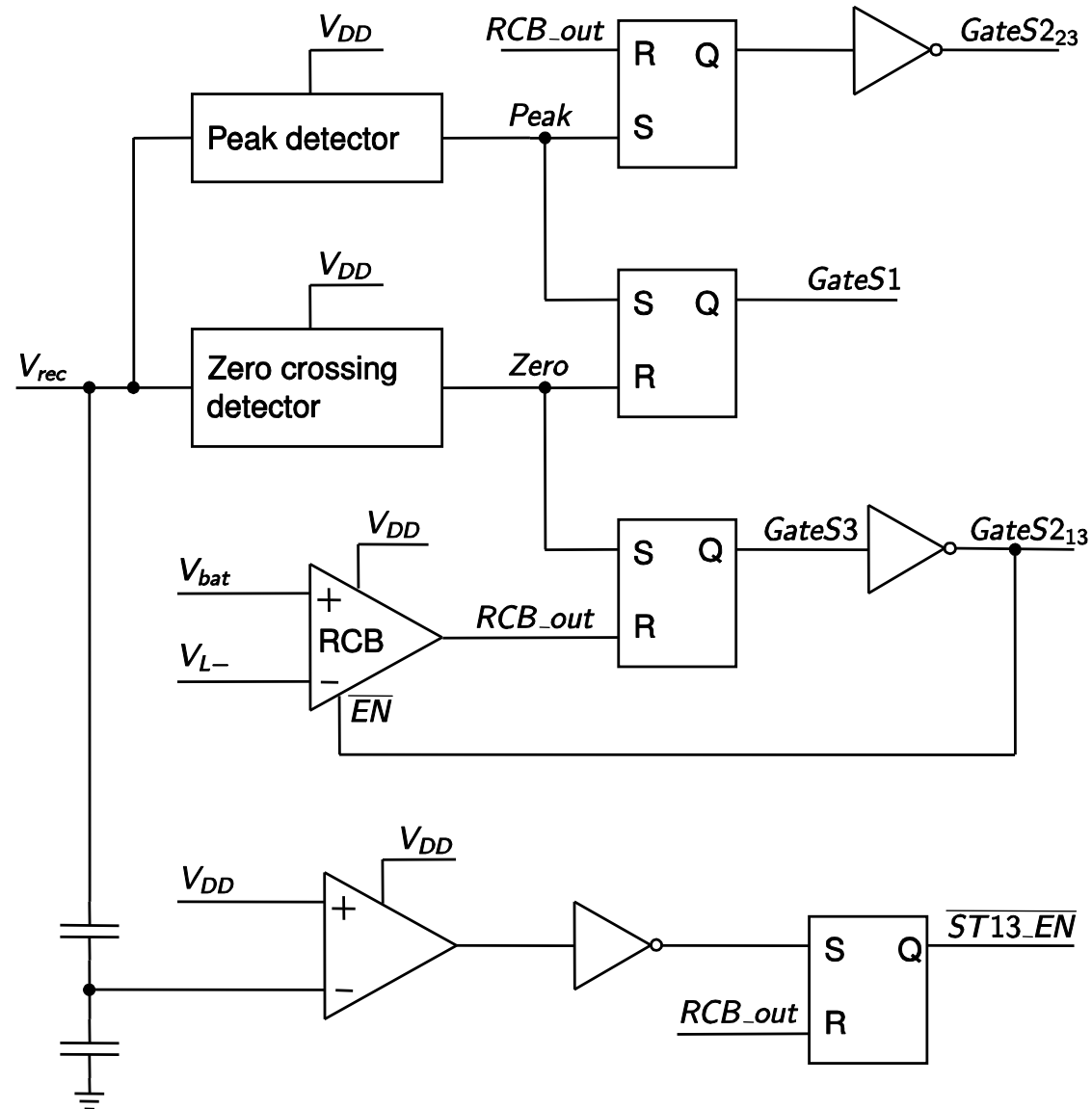


Peak detector



- Principle: Voltage-to-current conversion
- Series capacitor C_s is charged with I_s while V_{rec} rises
- When I_s falls below constant current I_{ref} , a peak pulse is generated, initiating transfer process
- After rising edge of peak pulse, C_s is discharged to be prepared for next cycle

HV circuit – Control circuit



HV circuit – Main

